

Mechanical and physical properties of screws

according to ISO 898, part 1

The mechanical properties are given for tests at room temperature.

| No. | Mechanical or physical property | Property class | | | | | | | | | | |
|-----|--|---|-------------------|-------------------|-------------------|-------------------|----------------------------------|------------------------------|---------------------|-------------------|-------------------|-------------------|
| | | 4.6 | 4.8 | 5.6 | 5.8 | 6.8 | 8.8 d ≤ 16 mm ^a | d > 16 mm ^b | 9.8 d ≤ 16 mm | 10.9 | 12.9/ 12.9 | |
| 1 | Tensile strength, R_m , MPa, [N/mm ²] | nom. ^c | 400 | 400 | 500 | 500 | 600 | 800 | 800 | 900 | 1000 | 1200 |
| | | min. | 400 | 420 | 500 | 520 | 600 | 800 | 800 | 900 | 1040 | 1220 |
| 2 | Lower yield strength, R_{eL}^d , MPa, [N/mm ²] | nom. ^c | 240 | – | 300 | – | – | – | – | – | – | – |
| | | min. | 240 | – | 300 | – | – | – | – | – | – | – |
| 3 | Stress at 0,2% non-proportional elongation $R_{p0,2}^e$, MPa, [N/mm ²] | nom. ^c | – | – | – | – | – | 640 | 640 | 720 | 900 | 1080 |
| | | min. | – | – | – | – | – | 640 | 660 | 720 | 940 | 1100 |
| 4 | Stress at 0,0048 d non-proportional elongation for full-size fasteners R_{pf} , MPa, [N/mm ²] | nom. ^c | – | 320 | – | 400 | 480 | – | – | – | – | – |
| | | min. | – | 340 ^g | – | 420 ^g | 480 ^g | – | – | – | – | – |
| 5 | Stress under proof load, $S_{p,1}^f$, MPa, [N/mm ²] | nom. | 225 | 310 | 280 | 380 | 440 | 580 | 600 | 650 | 830 | 970 |
| | | Proof strength ratio $S_{p,nom}/R_{eL, min}$ or $S_{p,nom}/R_{p0,2, min}$ or $S_{p,nom}/R_{pf, min}$ | 0,94 | 0,91 | 0,93 | 0,90 | 0,92 | 0,91 | 0,91 | 0,90 | 0,88 | 0,88 |
| 6 | Percentage elongation after fracture for machined test pieces, A, % | min. | 22 | – | 20 | – | – | 12 | 12 | 10 | 9 | 8 |
| 7 | Percentage reduction of area after fracture for machined test pieces, Z, % | min. | – | – | – | – | – | 52 | 52 | 48 | 48 | 44 |
| 8 | Elongation after fracture for full-size fasteners, A_f (see also ISO 898-1 Annex C) | min. | – | 0,24 | – | 0,22 | 0,20 | – | – | – | – | – |
| 9 | Head soundness | no fracture | | | | | | | | | | |
| 10 | Vickers hardness, HV F ≥ 98 N | min. | 120 | 130 | 155 | 160 | 190 | 250 | 255 | 290 | 320 | 385 |
| | | max. | 220 ^h | 220 ^h | 220 ^h | 220 ^h | 250 | 320 | 335 | 360 | 380 | 435 |
| 11 | Brinell hardness, HBW F = 30 D ² | min. | 114 | 124 | 147 | 152 | 181 | 238 | 242 | 276 | 304 | 366 |
| | | max. | 209 ^h | 209 ^h | 209 ^h | 209 ^h | 238 | 304 | 318 | 342 | 361 | 414 |
| 12 | Rockwell hardness, HRB | min. | 67 | 71 | 79 | 82 | 89 | – | – | – | – | – |
| | | max. | 95,0 ^h | 95,0 ^h | 95,0 ^h | 95,0 ^h | 99,5 | – | – | – | – | – |
| | Rockwell hardness, HRC | min. | – | – | – | – | – | 22 | 23 | 28 | 32 | 39 |
| | | max. | – | – | – | – | – | 32 | 34 | 37 | 39 | 44 |
| 13 | Surface hardness, HV 0,3 | max. | – | – | – | – | – | h | h | h | h,i | h,j |
| 14 | Height of non-decarburized thread zone, E, mm | min. | – | – | – | – | – | $\frac{1}{2} H_t$ | $\frac{1}{2} H_t$ | $\frac{1}{2} H_t$ | $\frac{2}{3} H_t$ | $\frac{3}{4} H_t$ |
| | | Depth of complete decarburization in the thread, G, mm | max. | – | – | – | – | – | 0,015 | 0,015 | 0,015 | 0,015 |
| 15 | Reduction of hardness after retempering, HV | max. | – | – | – | – | – | 20 | 20 | 20 | 20 | 20 |
| 16 | Breaking torque, M_B Nm | min. | – | – | – | – | – | in accordance with ISO 898-7 | | | | |
| 17 | Impact strength K_{V}^{k-1} , J | min. | – | – | 27 | – | – | 27 | 27 | 27 | 27 | m |
| 18 | Surface integrity in accordance with | ISO 6157-1 ⁿ | | | | | | | | | | ISO 6157-3 |

^a Values do not apply for structural bolting.

^b For structural bolting d ≥ M12.

^c Nominal values are specified only for the purpose of the designation system for property classes. See clause 5.

^d In cases where the lower yield strength R_{eL} cannot be determined, it is permissible to measure the stress at 0,2% non-proportional elongation $R_{p0,2}$.

^e For the property classes 4.8, 5.8 and 6.8 the values for $R_{pf, min}$ are under investigation. The present values are given for calculation of the proof stress ratio only. They are not test values.

^f Proof loads are specified in tables F.006.

^g Hardness determined at the end of a fastener shall be 250 HV, 238 HB or 99,5 HRB maximum.

^h Surface hardness shall not be more than 30 Vickers points above the measured core hardness of the fastener when determination of both surface hardness and core hardness are carried out with HV 0,3.

ⁱ Any increase in hardness at the surface which indicates that the surface hardness exceeds 390 HV is not acceptable.

^j Any increase in hardness at the surface which indicates that the surface hardness exceeds 435 HV is not acceptable.

^k Values are determined at a test temperature of –20 °C.

^l Applies to d ≥ 16 mm.

^m Value for K_V is under investigation.

ⁿ Instead of ISO 6157-1, ISO 6157-3 may apply by agreement between the manufacturer and the purchaser.

Minimum ultimate tensile loads

according to ISO 898, part 1


Minimum ultimate tensile loads – ISO metric coarse pitch thread

| Thread ¹⁾ d | Nominal stress area $A_{s, nom}$ [mm ²] | Minimum ultimate tensile load $F_{m, min}$ ($A_{s, nom} \times R_{m, min}$) [N] | | | | | | | | |
|---------------------------|---|---|--------|---------------------|--------|--------|----------------------|--------|---------------------|-----------|
| | | Property class | | | | | | | | |
| | | 4.6 | 4.8 | 5.6 | 5.8 | 6.8 | 8.8 | 9.8 | 10.9 | 12.9/12.9 |
| M3 | 5,03 | 2010 | 2110 | 2510 | 2620 | 3020 | 4020 | 4530 | 5230 | 6140 |
| M3,5 | 6,78 | 2710 | 2850 | 3390 | 3530 | 4070 | 5420 | 6100 | 7050 | 8270 |
| M4 | 8,78 | 3510 | 3690 | 4390 | 4570 | 5270 | 7020 | 7900 | 9130 | 10700 |
| M5 | 14,2 | 5680 | 5960 | 7100 | 7380 | 8520 | 11350 | 12800 | 14800 | 17300 |
| M6 | 20,1 | 8040 | 8440 | 10000 | 10400 | 12100 | 16100 | 18100 | 20900 | 24500 |
| M7 | 28,9 | 11600 | 12100 | 14400 | 15000 | 17300 | 23100 | 26000 | 30100 | 35300 |
| M8 | 36,6 | 14600 ²⁾ | 15400 | 18300 ²⁾ | 19000 | 22000 | 29200 ²⁾ | 32900 | 38100 ²⁾ | 44600 |
| M10 | 58,0 | 23200 ²⁾ | 24400 | 29000 ²⁾ | 30200 | 34800 | 46400 ²⁾ | 52200 | 60300 ²⁾ | 70800 |
| M12 | 84,3 | 33700 | 35400 | 42200 | 43800 | 50600 | 67400 ³⁾ | 75900 | 87700 | 103000 |
| M14 | 115 | 46000 | 48300 | 57500 | 59800 | 69000 | 92000 ³⁾ | 104000 | 120000 | 140000 |
| M16 | 157 | 62800 | 65900 | 78500 | 81600 | 94000 | 125000 ³⁾ | 141000 | 163000 | 192000 |
| M18 | 192 | 76800 | 80600 | 96000 | 99800 | 115000 | 159000 | – | 200000 | 234000 |
| M20 | 245 | 98000 | 103000 | 122000 | 127000 | 147000 | 203000 | – | 255000 | 299000 |
| M22 | 303 | 121000 | 127000 | 152000 | 158000 | 182000 | 252000 | – | 315000 | 370000 |
| M24 | 353 | 141000 | 148000 | 176000 | 184000 | 212000 | 293000 | – | 367000 | 431000 |
| M27 | 459 | 184000 | 193000 | 230000 | 239000 | 275000 | 381000 | – | 477000 | 560000 |
| M30 | 561 | 224000 | 236000 | 280000 | 292000 | 337000 | 466000 | – | 583000 | 684000 |
| M33 | 694 | 278000 | 292000 | 347000 | 361000 | 416000 | 576000 | – | 722000 | 847000 |
| M36 | 817 | 327000 | 343000 | 408000 | 425000 | 490000 | 678000 | – | 850000 | 997000 |
| M39 | 976 | 390000 | 410000 | 488000 | 508000 | 586000 | 810000 | – | 1020000 | 1200000 |

¹⁾ Where no thread pitch is indicated in a thread designation, coarse pitch is specified.

²⁾ For fasteners with thread tolerance 6az according to ISO 965-4 subject to hot dip galvanizing, reduced values in accordance with ISO 10684.

³⁾ For structural bolting 70 000 N (for M12), 95 500 N (for M14) and 130 000 N (for M16).

 To calculate the nominal stress area $A_{s, nom}$
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Minimum ultimate tensile loads – ISO metric fine pitch thread

| Thread d x P | Nominal stress area $A_{s, nom}$ [mm ²] | Minimum ultimate tensile load $F_{m, min}$ ($A_{s, nom} \times R_{m, min}$) [N] | | | | | | | | |
|-----------------|---|---|--------|--------|--------|--------|--------|--------|---------|-----------|
| | | Property class | | | | | | | | |
| | | 4.6 | 4.8 | 5.6 | 5.8 | 6.8 | 8.8 | 9.8 | 10.9 | 12.9/12.9 |
| M8x1 | 39,2 | 15700 | 16500 | 19600 | 20400 | 23500 | 31360 | 35300 | 40800 | 47800 |
| M10x1 | 64,5 | 25800 | 27100 | 32300 | 33500 | 38700 | 51600 | 58100 | 67100 | 78700 |
| M10x1,25 | 61,2 | 24500 | 25700 | 30600 | 31800 | 36700 | 49000 | 55100 | 63600 | 74700 |
| M12x1,25 | 92,1 | 36800 | 38700 | 46100 | 47900 | 55300 | 73700 | 82900 | 95800 | 112000 |
| M12x1,5 | 88,1 | 35200 | 37000 | 44100 | 45800 | 52900 | 70500 | 79300 | 91600 | 107000 |
| M14x1,5 | 125 | 50000 | 52500 | 62500 | 65000 | 75000 | 100000 | 112000 | 130000 | 152000 |
| M16x1,5 | 167 | 66800 | 70100 | 83500 | 86800 | 100000 | 134000 | 150000 | 174000 | 204000 |
| M18x1,5 | 216 | 86400 | 90700 | 108000 | 112000 | 130000 | 179000 | – | 225000 | 264000 |
| M20x1,5 | 272 | 109000 | 114000 | 136000 | 141000 | 163000 | 226000 | – | 283000 | 332000 |
| M22x1,5 | 333 | 133000 | 140000 | 166000 | 173000 | 200000 | 276000 | – | 346000 | 406000 |
| M24x2 | 384 | 154000 | 161000 | 192000 | 200000 | 230000 | 319000 | – | 399000 | 469000 |
| M27x2 | 496 | 198000 | 208000 | 248000 | 258000 | 298000 | 412000 | – | 516000 | 605000 |
| M30x2 | 621 | 248000 | 261000 | 310000 | 323000 | 373000 | 515000 | – | 646000 | 758000 |
| M33x2 | 761 | 304000 | 320000 | 380000 | 396000 | 457000 | 632000 | – | 791000 | 928000 |
| M36x3 | 865 | 346000 | 363000 | 432000 | 450000 | 519000 | 718000 | – | 900000 | 1055000 |
| M39x3 | 1030 | 412000 | 433000 | 515000 | 536000 | 618000 | 855000 | – | 1070000 | 1260000 |

Proof loads of screws

according to ISO 898, part 1

Proof loads – ISO metric coarse pitch thread

| Thread ¹⁾ d | Nominal stress area $A_{s, \text{nom}}$ [mm ²] | Proof load $F_p (A_{s, \text{nom}} \times S_{p, \text{nom}}^{4)})$ [N] | | | | | | | | | |
|---------------------------|--|--|--------|---------------------|--------|--------|---------------------|--------|---------------------|-----------|--|
| | | Property class | | | | | | | | | |
| | | 4.6 | 4.8 | 5.6 | 5.8 | 6.8 | 8.8 | 9.8 | 10.9 | 12.9/12.9 | |
| M3 | 5,03 | 1130 | 1560 | 1410 | 1910 | 2210 | 2920 | 3270 | 4180 | 4880 | |
| M3,5 | 6,78 | 1530 | 2100 | 1900 | 2580 | 2980 | 3940 | 4410 | 5630 | 6580 | |
| M4 | 8,78 | 1980 | 2720 | 2460 | 3340 | 3860 | 5100 | 5710 | 7290 | 8520 | |
| M5 | 14,2 | 3200 | 4400 | 3980 | 5400 | 6250 | 8230 | 9230 | 11800 | 13800 | |
| M6 | 20,1 | 4520 | 6230 | 5630 | 7640 | 8840 | 11600 | 13100 | 16700 | 19500 | |
| M7 | 28,9 | 6500 | 8960 | 8090 | 11000 | 12700 | 16800 | 18800 | 24000 | 28000 | |
| M8 | 36,6 | 8240 ²⁾ | 11400 | 10200 ²⁾ | 13900 | 16100 | 21200 ²⁾ | 23800 | 30400 ²⁾ | 35500 | |
| M10 | 58,0 | 13000 ²⁾ | 18000 | 16200 ²⁾ | 22000 | 25500 | 33700 ²⁾ | 37700 | 48100 ²⁾ | 56300 | |
| M12 | 84,3 | 19000 | 26100 | 23600 | 32000 | 37100 | 48900 ³⁾ | 54800 | 70000 | 81800 | |
| M14 | 115 | 25900 | 35600 | 32200 | 43700 | 50600 | 66700 ³⁾ | 74800 | 95500 | 112000 | |
| M16 | 157 | 35300 | 48700 | 44000 | 59700 | 69100 | 91000 ³⁾ | 102000 | 130000 | 152000 | |
| M18 | 192 | 43200 | 59500 | 53800 | 73000 | 84500 | 115000 | – | 159000 | 186000 | |
| M20 | 245 | 55100 | 76000 | 68600 | 93100 | 108000 | 147000 | – | 203000 | 238000 | |
| M22 | 303 | 68200 | 93900 | 84800 | 115000 | 133000 | 182000 | – | 252000 | 294000 | |
| M24 | 353 | 79400 | 109000 | 98800 | 134000 | 155000 | 212000 | – | 293000 | 342000 | |
| M27 | 459 | 103000 | 142000 | 128000 | 174000 | 202000 | 275000 | – | 381000 | 445000 | |
| M30 | 561 | 126000 | 174000 | 157000 | 213000 | 247000 | 337000 | – | 466000 | 544000 | |
| M33 | 694 | 156000 | 215000 | 194000 | 264000 | 305000 | 416000 | – | 576000 | 673000 | |
| M36 | 817 | 184000 | 253000 | 229000 | 310000 | 359000 | 490000 | – | 678000 | 792000 | |
| M39 | 976 | 220000 | 303000 | 273000 | 371000 | 429000 | 586000 | – | 810000 | 947000 | |

¹⁾ Where no thread pitch is indicated in a thread designation, coarse pitch is specified.

²⁾ For fasteners with thread tolerance 6az according to ISO 965-4 subject to hot dip galvanizing, reduced values in accordance with ISO 10684.

³⁾ For structural bolting 50 700 N (for M12), 68 800 N (for M14) and 94 500 N (for M16).

⁴⁾ Value for stress under proof load $S_{p, \text{nom}}$ and their relation to stress at non-proportional elongation see page F.004, No. 5 in table.

▶ To calculate the nominal stress area $A_{s, \text{nom}}$
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Proof loads – ISO metric fine pitch thread

| Thread d x P | Nominal stress area $A_{s, \text{nom}}$ [mm ²] | Proof load $F_p (A_{s, \text{nom}} \times S_{p, \text{nom}})$ [N] | | | | | | | | | |
|-----------------|--|---|--------|--------|--------|--------|--------|--------|--------|-----------|--|
| | | Property class | | | | | | | | | |
| | | 4.6 | 4.8 | 5.6 | 5.8 | 6.8 | 8.8 | 9.8 | 10.9 | 12.9/12.9 | |
| M8x1 | 39,2 | 8820 | 12200 | 11000 | 14900 | 17200 | 22700 | 25500 | 32500 | 38000 | |
| M10x1,25 | 61,2 | 13800 | 19000 | 17100 | 23300 | 26900 | 35500 | 39800 | 50800 | 59400 | |
| M10x1 | 64,5 | 14500 | 20000 | 18100 | 24500 | 28400 | 37400 | 41900 | 53500 | 62700 | |
| M12x1,25 | 92,1 | 20700 | 28600 | 25800 | 35000 | 40500 | 53400 | 59900 | 76400 | 89300 | |
| M12x1,5 | 88,1 | 19800 | 27300 | 24700 | 33500 | 38800 | 51100 | 57300 | 73100 | 85500 | |
| M14x1,5 | 125 | 28100 | 38800 | 35000 | 47500 | 55000 | 72500 | 81200 | 104000 | 121000 | |
| M16x1,5 | 167 | 37600 | 51800 | 46800 | 63500 | 73500 | 96900 | 109000 | 139000 | 162000 | |
| M18x1,5 | 216 | 48600 | 67000 | 60500 | 82100 | 95000 | 130000 | – | 179000 | 210000 | |
| M20x1,5 | 272 | 61200 | 84300 | 76200 | 103000 | 120000 | 163000 | – | 226000 | 264000 | |
| M22x1,5 | 333 | 74900 | 103000 | 93200 | 126000 | 146000 | 200000 | – | 276000 | 323000 | |
| M24x2 | 384 | 86400 | 119000 | 108000 | 146000 | 169000 | 230000 | – | 319000 | 372000 | |
| M27x2 | 496 | 112000 | 154000 | 139000 | 188000 | 218000 | 298000 | – | 412000 | 481000 | |
| M30x2 | 621 | 140000 | 192000 | 174000 | 236000 | 273000 | 373000 | – | 515000 | 602000 | |
| M33x2 | 761 | 171000 | 236000 | 213000 | 289000 | 335000 | 457000 | – | 632000 | 738000 | |
| M36x3 | 865 | 195000 | 268000 | 242000 | 329000 | 381000 | 519000 | – | 718000 | 839000 | |
| M39x3 | 1030 | 232000 | 319000 | 288000 | 391000 | 453000 | 618000 | – | 855000 | 999000 | |

Materials, heat treatment, chemical compositions

according to ISO 898, part 1

Steels

| Property class | Material and heat treatment | Chemical composition limits (cast analysis, %) ¹⁾ | | | | | Tempering temperature °C |
|----------------------------|---|--|------|-------|-------|-----------------|--------------------------|
| | | C | | P | S | B ²⁾ | |
| | | min. | max. | max. | max. | max. | |
| 4.6 ^{3), 4)} | Carbon steel or carbon steel with additives | – | 0,55 | 0,05 | 0,06 | not specified | – |
| 4.8 ⁴⁾ | | | | | | | |
| 5.6 ⁵⁾ | | 0,13 | 0,55 | 0,05 | 0,06 | | |
| 5.8 ⁴⁾ | | – | 0,55 | 0,05 | 0,06 | | |
| 6.8 ⁴⁾ | | 0,15 | 0,55 | 0,05 | 0,06 | | |
| 8.8 ⁶⁾ | Carbon steel with additives (e.g. Boron or Mn or Cr), quenched and tempered | 0,15 ⁵⁾ | 0,40 | 0,025 | 0,025 | 0,003 | 425 |
| | or Carbon steel, quenched and tempered | 0,25 | 0,55 | 0,025 | 0,025 | | |
| | or Alloyed steel, quenched and tempered ⁷⁾ | 0,20 | 0,55 | 0,025 | 0,025 | | |
| | | | | | | | |
| 9.8 ⁶⁾ | Carbon steel with additives (e.g. Boron or Mn or Cr), quenched and tempered | 0,15 ⁵⁾ | 0,40 | 0,025 | 0,025 | 0,003 | 425 |
| | or Carbon steel, quenched and tempered | 0,25 | 0,55 | 0,025 | 0,025 | | |
| | or Alloyed steel, quenched and tempered ⁷⁾ | 0,20 | 0,55 | 0,025 | 0,025 | | |
| | | | | | | | |
| 10.9 ⁶⁾ | Carbon steel with additives (e.g. Boron, Mn or Cr), quenched and tempered | 0,20 ⁵⁾ | 0,55 | 0,025 | 0,025 | 0,003 | 425 |
| | or Carbon steel, quenched and tempered | 0,25 | 0,55 | 0,025 | 0,025 | | |
| | or Alloyed steel, quenched and tempered ⁷⁾ | 0,20 | 0,55 | 0,025 | 0,025 | | |
| | | | | | | | |
| 12.9 ^{6), 8), 9)} | Alloyed steel, quenched and tempered ⁷⁾ | 0,30 | 0,50 | 0,025 | 0,025 | 0,003 | 425 |
| 12.9 ^{6), 8), 9)} | Carbon steel with additives (e.g. Boron, Mn or Cr or Molybdenum), quenched and tempered | 0,28 | 0,50 | 0,025 | 0,025 | 0,003 | 380 |

¹⁾ In case of dispute, the product analysis applies.

²⁾ Boron content can reach 0,005 %, provided that non-effective boron is controlled by addition of titanium and/or aluminum.

³⁾ For cold forged fasteners of property classes 4.6 and 5.6, heat treatment of the wire used for cold forging or of the cold forged fastener itself may be necessary to achieve required ductility.

⁴⁾ Free cutting steel is allowed for these property classes with the following maximum sulphur, phosphorus and lead contents: sulphur 0,34%; phosphorus 0,11 %; lead 0,35 %.

⁵⁾ In case of plain carbon boron steel with a carbon content below 0,25 % (cast analysis), the minimum manganese content shall be 0,6 % for property class 8.8 and 0,7 % for 9.8 and 10.9.

⁶⁾ For the materials of these property classes, there shall be a sufficient hardenability to ensure a structure consisting of approximately 90 % martensite in the core of the threaded sections for the fasteners in the «as-hardened» condition before tempering.

⁷⁾ This alloy steel shall contain at least one of the following elements in the minimum quantity given: chromium 0,3 %, nickel 0,3 %, molybdenum 0,2 %, vanadium 0,1 %. Where elements are specified in combinations of two, three or four and have alloy contents less than those given above, the limit value to be applied for class determination is 70 % of the sum of the individual limit values shown above for the two, three or four elements concerned.

⁸⁾ A metallographically detectable white phosphorous enriched layer is not permitted for property class 12.9/12.9. It shall be detected by a suitable test method.

⁹⁾ Caution is advised when the use of property class 12.9/12.9 is considered. The capability of the fastener manufacturer, the service conditions and the wrenching methods should be considered. Environments may cause stress corrosion cracking of fasteners as processed as well as those coated.

Characteristics at elevated temperatures

according to ISO 898, part 1

Influence of elevated temperatures on mechanical properties of fasteners

Elevated temperatures can cause changes in the mechanical properties and in the functional performance of a fastener.

Up to typical service temperatures of 150 °C, no detrimental effects due to a change of mechanical properties of fasteners are known. At temperatures over 150 °C and up to a maximum temperature of 300 °C, the functional performance of fasteners should be ensured by careful examination.

With increasing temperatures, a progressive

- reduction of lower yield strength or stress at 0,2% non-proportional elongation or stress at 0,0048 d non-proportional elongation for finished fasteners, and
- reduction of tensile strength can be experienced. The continuous operating of fasteners at elevated service temperatures can result in stress relaxation, which increases with higher temperatures. Stress relaxation accompanies a loss of clamp force.

Work-hardened fasteners (property classes 4.8, 5.8, 6.8) are more sensitive with regard to stress relaxation compared with quenched and tempered or stress-relieved fasteners.

Care should be taken when lead-containing steels are used for fasteners at elevated temperatures. For such fasteners, a risk of liquid metal embrittlement (LME) should be taken into consideration when the service temperature is in the range of the melting point of lead.

Information for example, in EN 10269 and in ASTM F2281.

Characteristics at higher strength (if $\geq 1000 \text{ N/mm}^2$)

Influence of higher screw property class under comprehension of the mechanical stress and environmental conditions.

▶ Risk of hydrogen embrittlement
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